



# CO<sub>2</sub> capture using mesoporous alumina prepared by a sol–gel process

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## ABSTRACT

Mesoporous alumina (MA) having high surface area (812 m<sup>2</sup>/g) and large pore volume (0.83 cm<sup>3</sup>/g) with a narrow pore size distribution was prepared by a simple sol–gel process. The as-prepared MA was characterized by XRD, N<sub>2</sub> adsorption–desorption isotherms, and transmission electron microscopy (TEM). The CO<sub>2</sub> adsorption performance of MA was tested under both low (<1 bar) pressure using a static volumetric system and high pressure (<30 bar) conditions using a gravimetric system. MA demonstrated a CO<sub>2</sub> capture capacity of ca. 52 mg/g<sub>adsorbent</sub> at 1 bar, a value higher than that of a commercial alumina or 3-aminopropyltrimethoxysilane-grafted MCM-41. High pressure (0–30 bar) CO<sub>2</sub> adsorption increased in a sequence of commercial alumina < SBA-15 < zeolite 13X < MA. Static adsorption and breakthrough experiments showed that MA offers high separation efficiency for CO<sub>2</sub> against N<sub>2</sub>. CO<sub>2</sub> desorption at different temperatures was evaluated in order to identify regeneration conditions of MA after CO<sub>2</sub> adsorption. PEI (polyethylenimine)-impregnated MA was also prepared and tested as a CO<sub>2</sub> sorbent. The hybrid sorbent material achieved higher CO<sub>2</sub> capture capacity (120 mg/g<sub>sorbent</sub>) than MA alone, with a level comparable to the sorption capacities of PEI functionalized mesoporous silica materials reported to date. Both as-prepared and PEI-impregnated MA exhibited stable adsorption–desorption behaviour during 5 consecutive test cycles.

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## 1. Introduction

At present, the discharge of CO<sub>2</sub> into the atmosphere by the consumption of increasing amounts of fossil fuels is believed to be causing a serious global warming problem. Accordingly, much effort has been made over the last decade to develop various chemical and physical methods for CO<sub>2</sub> capture and sequestration (CCS) as a means of alleviating this problem [1]. Among these approaches, porous solid adsorbents have been widely investigated as a medium for CO<sub>2</sub> capture, as researchers attempt to exploit their large accessible surface areas and large pore volumes.

Alumina has been widely used for catalysis and adsorption processes. It is proved by several studies dealing with the infrared spectra of CO<sub>2</sub> adsorbed on alumina [2–5] that there are both physical and chemical adsorption sites for CO<sub>2</sub> on alumina surface, but only limited research has been reported on transitional alumina or activated aluminas as CO<sub>2</sub> adsorbents; Rosynek studied the CO<sub>2</sub> adsorption on commercial  $\gamma$ -alumina [6]; Mao and Vannice studied CO<sub>2</sub> adsorption property of  $\alpha$ -alumina [7]; and Li et al. studied the binary adsorption equilibrium of CO<sub>2</sub> and water vapor on activated alumina [8]. Alkali metal oxide and salts-modified alumina have also been studied for CO<sub>2</sub> capturing agents; Horiuchi et al. modi-

fied  $\gamma$ -alumina by adding basic metal oxides and studied its CO<sub>2</sub> adsorption performance at elevated temperatures [9]; Zou et al. studied the adsorption of CO<sub>2</sub> on commercial basic aluminas containing ca. 5% Na [10]; Slaugh and Willis impregnated alkali salts on commercial alumina and studied CO<sub>2</sub> removal after calcination of the sample at 350–800 °C [11]; and Okunev et al. studied the sorption of CO<sub>2</sub> from wet gases over K<sub>2</sub>CO<sub>3</sub> impregnated on porous alumina [12]. These aluminas usually exhibit surface areas lower than 350–400 m<sup>2</sup>/g, and have broad pore size distributions [13].

On the other hand, there has been no investigation of CO<sub>2</sub> adsorption by mesoporous alumina (MA). Compared to those transitional or activated aluminas tested for CO<sub>2</sub> adsorption so far, MA possesses significantly higher surface area and much narrower pore size distribution in the mesopore region [14]. Therefore, increased adsorption sites for CO<sub>2</sub> are expected in MA, which can lead to an improved CO<sub>2</sub> adsorption performance. In addition, the large pore volume and narrow pore size distribution in MA also would enable us to introduce a large amount of amine-type CO<sub>2</sub> capturing agent into its mesopores in a well dispersed manner, which can function as an effective hybrid type CO<sub>2</sub> sorbent. Various amine species are known to react with CO<sub>2</sub> via a carbamate formation mechanism; two molecules of amine species react with one molecule of CO<sub>2</sub> to form a carbamate species (2R-NH<sub>2</sub> + CO<sub>2</sub> → R-NH<sub>3</sub><sup>+</sup> + R-NHCOO<sup>-</sup>). A high quality hybrid CO<sub>2</sub> sorbent can be obtained if a suitable amine is chosen and introduced into the pore structure of a mesoporous material. For this purpose, we have been using

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PEI (polyethylenimine) as a CO<sub>2</sub>-capturing agent, since it has a high concentration of N which can interact with CO<sub>2</sub> molecules. It also has a higher boiling point than other amines, making it possible to achieve enhanced thermal stability of the hybrid material. Mesoporous silica has been extensively investigated as a support material for amine species [15–22], while no work to date has considered MA functionalized with amine species for CO<sub>2</sub> removal. It also has yet to be determined if the adsorption sites in MA alone can provide an additional contribution to CO<sub>2</sub> capture (i.e., excluding the contribution by PEI).

In this work, MA having desirable textural properties (high surface area and large pore volume) was synthesized via a simple sol–gel process. This as-prepared MA was systematically evaluated as a CO<sub>2</sub> adsorbent, and compared against the performances of commercial alumina and amine-grafted MCM-41. PEI-loaded MA was prepared by an impregnation method and the resultant hybrid material was also investigated as a CO<sub>2</sub> sorbent.

## 2. Experimental

### 2.1. Synthesis of MA

MA was synthesized via a sol–gel process reported by Zhang et al. [23]. Aluminum isopropoxide (Al(i-PrO)<sub>3</sub>) (41.68 g) was initially added into an alcohol solvent mixture (73.6 g ethanol and 72.2 g isopropanol) at 50 °C to obtain a milky sol. Distilled water (7.2 g) was then dropped into the mixture to promote hydrolysis of aluminum isopropoxide. The sol was subsequently stirred at room temperature for 9 h, heated in an oven at 70 °C for 24 h, followed by heating at 100 °C for 2 h. This gel was placed in an autoclave and heated at 120 °C for 12 h. Finally, the gel was washed with ethanol and dried.

### 2.2. PEI impregnation on MA

PEI was introduced into MA according to a procedure reported by Xu et al. [17]. The maximum amount of PEI that could be introduced into MA without exceeding the available pore volume was calculated based on the pore volume of MA (0.83 cm<sup>3</sup>/g) and the density of PEI (1.05 g/cm<sup>3</sup>). The resultant hybrid material was designated as PEI/MA in this work. In a typical preparation, 0.87 g PEI (Aldrich, average molecular weight of 600 by GPC, linear type, b.p. of 250 °C) was dissolved in methanol under stirring for about 15 min, after which 1 g of pretreated MA was added to the PEI/methanol solution in a glove box. The resultant slurry was continuously stirred for about 30 min and then heated at 70 °C for 16 h under reduced pressure (700 mmHg).

### 2.3. Amine grafting on MCM-41

MCM-41 was prepared according to the procedure reported by Beck et al. [24]. Dried MCM-41 (1.5 g) was added to 15 ml of toluene with stirring, and then 3-aminopropyltrimethoxysilane (0.92 g) was added to the mixture, stirred for 6 h at room temperature, and refluxed for 4 h at 383 K. The product was filtered and washed with ethanol and dried at 343 K under vacuum.

### 2.4. Characterization of the materials prepared

The XRD patterns were obtained on a Rigaku diffractometer using Cu K $\alpha$  ( $\lambda = 1.54 \text{ \AA}$ ) radiation. Nitrogen adsorption–desorption isotherms were measured on a Micromeritics ASAP-2000 sorptometer at liquid nitrogen temperature. The specific surface areas of samples were calculated by the BET method and the pore diameters and pore size distributions were evaluated from the desorption branch of the isotherm based on the BJH (Barrett–Joyner–Halenda)

model. High-resolution TEM images were obtained on an EM-2100F model operated at 200 kV. An elemental analysis (EA) was carried out for the amine-grafted and PEI-impregnated samples.

### 2.5. CO<sub>2</sub> adsorption–desorption measurement

The ambient pressure CO<sub>2</sub> adsorption isotherms were obtained using a BEL adsorption instrument (BELsorp-mini). Vacuum was introduced in the pretreatment process. MA and commercial  $\gamma$ -alumina were pretreated at 200 °C while amine-grafted MCM-41 was pretreated at 100 °C. Adsorption experiments were carried out using ultra high purity CO<sub>2</sub> in a pressure range of 0–1 bar at 298 K. For MA, adsorption at 273 K was also tested. Initially, all the experimental adsorption data were fitted to the Langmuir–Freundlich equation, and then the heats of adsorption were calculated by applying the Clausius–Clapeyron equation:

$$\left[ \frac{\partial \ln P}{\partial (1/T)} \right]_q = \frac{-\Delta H}{R}$$

where  $P$  is pressure,  $T$  is temperature,  $q$  is the amount adsorbed,  $R$  is the gas constant and  $\Delta H$  denotes the heat of adsorption. The high pressure CO<sub>2</sub> adsorption isotherms were obtained using a magnetic suspension balance (Rubotherm, Germany) with in situ density measurements in a closed system. Before measuring the CO<sub>2</sub> adsorption capacity, the buoyancy effect was corrected in ultra high purity He. High-pressure adsorption was carried out using ultra high purity CO<sub>2</sub> in a pressure range of 0–30 bar at 298 K.

CO<sub>2</sub> desorption and adsorption/desorption cycle experiment was conducted by a TGA unit (SCINCO thermal gravimeter S-1000) connected to a gas flow panel. Helium (ultra high purity, U-Sung) was used as a purge gas in the initial activation and desorption experiments, and adsorption was carried out using ultra high purity CO<sub>2</sub>. A feed flow rate of 30 ml/min was controlled with a MFC to the sample chamber.

The gas-separation efficiency of MA was tested by breakthrough experiments using a CO<sub>2</sub>/N<sub>2</sub> (15:85, v/v) gas mixture at room temperature. For this purpose, 1 g of pretreated MA was packed into a U-type stainless-steel column, and the gas mixture was fed into the column at a flow rate of 10 ml/min. The relative amounts of the gases passing through the column were monitored on a Hiden Analytical HPR20 gas analysis system. The relative intensity of each gas component was normalized to the same level by purging gas mixtures through the bypass before they passed through the column.

## 3. Results and discussion

### 3.1. Physical properties of MA

Fig. 1 shows the XRD patterns of the MA prepared samples. The single broad diffraction peak appearing at about  $2\theta = 1.5^\circ$  in Fig. 1(a) confirms the mesoporous structure of MA. The inset of the figure is a high-resolution TEM image of MA, which shows a disordered wormhole pore structure. As shown in Fig. 1(b), after PEI impregnation, the location of the characteristic Bragg diffraction peak remained nearly constant, but the intensity of the diffraction peak decreased substantially, indicating that PEI was successfully introduced into the channels of the alumina support [17].

Fig. 2 shows the N<sub>2</sub> adsorption–desorption isotherms of MA and commercial  $\gamma$ -alumina measured at 77 K. Both samples showed type IV isotherms with hysteresis loops. As shown in the inset, the pore size distribution of MA is much narrower than that of the commercial  $\gamma$ -alumina. Textural properties of the MA and the commercial  $\gamma$ -alumina are presented in Table 1. The average pore size of MA estimated using the desorption branch of the isotherm is smaller than that of commercial  $\gamma$ -alumina (4.1 vs 6.6 nm); how-

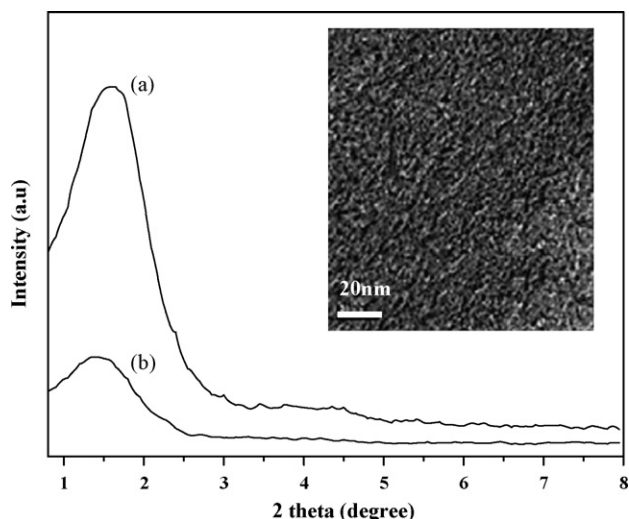


Fig. 1. XRD patterns of the MA samples prepared: (a) MA and (b) PEI/MA. The inset is the TEM image of MA.

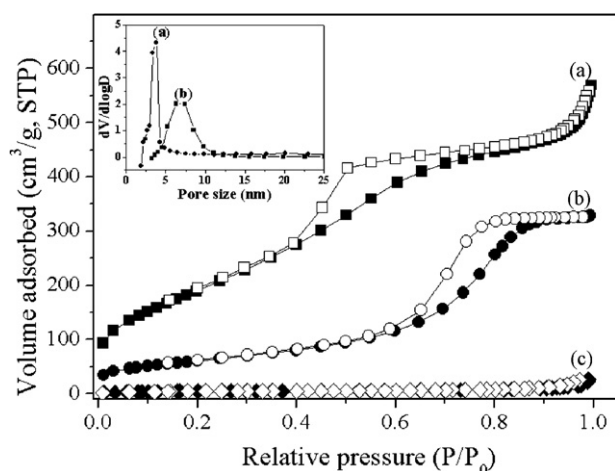


Fig. 2. N<sub>2</sub> adsorption–desorption isotherms: (a) MA, (b) commercial  $\gamma$ -alumina, and (c) PEI/MA. The insets are pore size distribution curves of (a) MA and (b) commercial  $\gamma$ -alumina.

ever, the surface area and pore volume of MA are substantially larger than those of commercial  $\gamma$ -alumina (812 vs 220 m<sup>2</sup>/g for surface area, and 0.83 vs 0.54 cm<sup>3</sup>/g for pore volume). These textural properties of MA are comparable to those of previously reported results for mesoporous silica materials [19]. Fig. 2(c) shows the N<sub>2</sub> adsorption–desorption isotherms of PEI/MA. After introducing PEI on to MA, the mesopores were virtually filled with PEI, resulting in a type II isotherm. This is consistent with the BET surface area data summarized in Table 1; the BET surface area and the resid-

Table 1  
Textural properties of adsorbents used.

Samples	$S_{\text{BET}}$ (m <sup>2</sup> /g)	$V_t$ (cm <sup>3</sup> /g) <sup>a</sup>	$D_p$ (nm) <sup>b</sup>
$\gamma$ -Alumina	220	0.54	6.6
MA	812	0.83	4.1
PEI/MA	2	0.03	–
MCM-41	1050	0.91	2.9
SBA-15	753	1.0	5.6
Zeolite 13X	893	0.34	–

<sup>a</sup> Total pore volume by N<sub>2</sub> adsorption at  $P/P_0 = 0.99$ .

<sup>b</sup> Average pore size estimated from the desorption branch of the isotherms based on the BJH (Barrett–Joyner–Halenda) model.

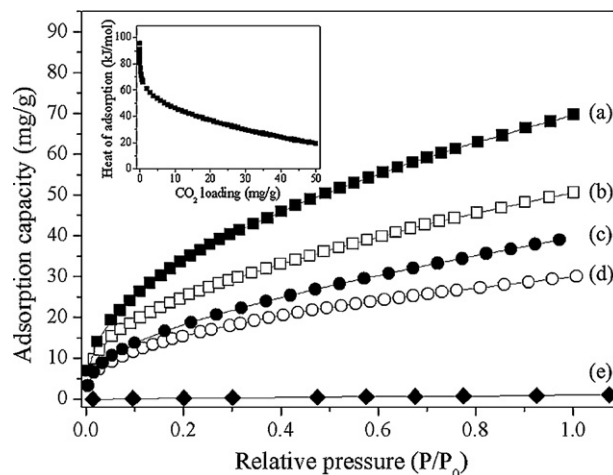


Fig. 3. CO<sub>2</sub> adsorption isotherms of (a) MA at 273 K, (b) MA at 298 K, (c) amine grafted MCM-41 at 298 K, (d) commercial  $\gamma$ -alumina at 298 K, (e) N<sub>2</sub> adsorption isotherm of MA at 298 K. The inset is the isosteric heat of adsorption estimated as a function of the amount of CO<sub>2</sub> adsorbed by MA.

ual pore volumes for PEI/MA were only 2 m<sup>2</sup>/g and 0.03 cm<sup>3</sup>/g, respectively.

### 3.2. CO<sub>2</sub> adsorption by MA

Initially, we conducted a low pressure static CO<sub>2</sub> adsorption experiment at 298 K. Fig. 3(b) and (d) shows the adsorption isotherms of MA and commercial  $\gamma$ -alumina, respectively. The adsorption capacity of MA is noticeably higher than that of commercial  $\gamma$ -alumina (52 vs 30 mg CO<sub>2</sub>/g<sub>adsorbent</sub>). This can be attributed to the high surface area of MA, which leads to more adsorption sites exposed to CO<sub>2</sub>. We also prepared an amine-grafted mesoporous silica sample, which is well known as a CO<sub>2</sub> sorbent, and evaluated its sorption capacity for comparison. As shown in Fig. 3(c), 3-aminopropyltrimethoxysilane-grafted MCM-41 (N loading: 28 mg/g<sub>adsorbent</sub>) exhibited a CO<sub>2</sub> sorption capacity of ca. 40 mg/g<sub>adsorbent</sub>, which is still below the capacity of as-prepared MA. Thus, MA alone without any functionalization proved to have a significant CO<sub>2</sub> adsorption capacity. To have an idea about the adsorption capacities of competing adsorbents for CO<sub>2</sub>, CO<sub>2</sub> capture capacities by MA in this work and other adsorbent materials reported in literature were compared in Table 2.

We further carried out CO<sub>2</sub> adsorption at high pressure conditions of up to 30 bar, and SBA-15, zeolite 13X, and commercial  $\gamma$ -alumina were also evaluated for comparison. Fig. 4 shows the high pressure CO<sub>2</sub> adsorption isotherms of these four materials. Mesoporous silica SBA-15 and commercial  $\gamma$ -alumina were in-

ferior to MA. MA was then tested for CO<sub>2</sub> adsorption at high pressure conditions of up to 30 bar, and SBA-15, zeolite 13X, and commercial  $\gamma$ -alumina were also evaluated for comparison. Fig. 4 shows the high pressure CO<sub>2</sub> adsorption isotherms of these four materials. Mesoporous silica SBA-15 and commercial  $\gamma$ -alumina were in-

**Table 2**  
CO<sub>2</sub> capture capacities and heats of adsorption of sorbents.

Sample	Temp. (°C)	CO <sub>2</sub> uptake (mg/g)		$\Delta H$ (kJ/mol)	Reference
		1 bar	30 bar		
$\gamma$ -Alumina	25	30	259	–	Present work
MA	25	52	381	20–98	Present work
SBA-15	25	21	260	–	Present work
Zeolite 13X	25	231	299	–	Present work
Amine-MCM-41 <sup>a</sup>	25	40	–	–	Present work
PEI/MA	75	120	–	–	Present work
Na-ZSM-5	24	81	–	29–51	[25]
Na-Zeolite $\beta$	25	120	–	29–57	[26]
CuBTC	22	220	–	28–35	[27]
MOF508b	30	88	–	17–20	[28]
ITQ-6/AP <sup>a</sup>	20	53	–	22–65	[29]
APS-MCM-48 <sup>b</sup>	25	35	–	–	[30]
TRI-PE-MCM-41 <sup>c</sup>	25	122	–	20–92	[31]

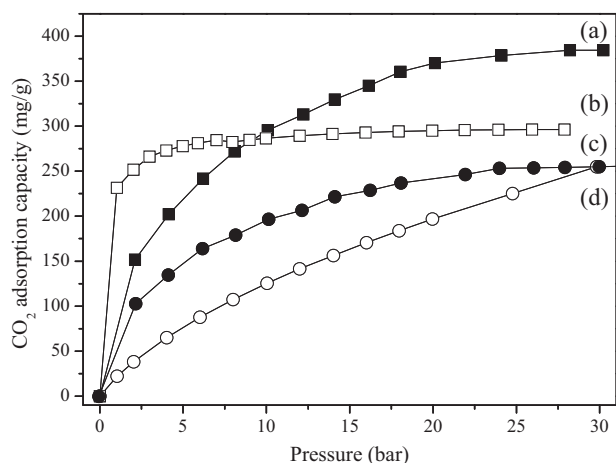
<sup>a</sup> 3-Aminopropyltrimethoxysilane as amine grafting source.

<sup>b</sup> 3-Aminopropyltriethoxysilane as amine grafting source.

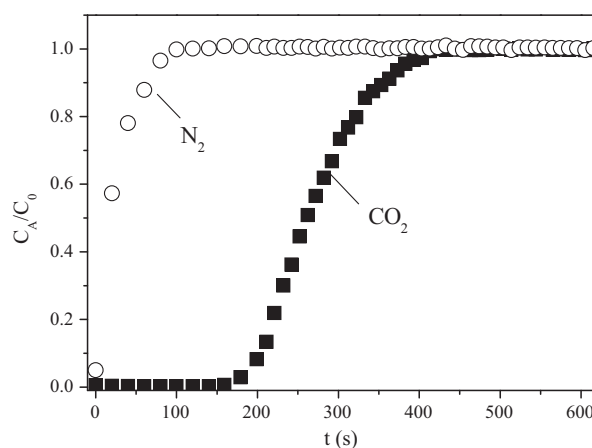
<sup>c</sup> 2-[2-(3-Trimethoxysilylpropylamino)ethylamino]ethylamine as amine grafting source.

rior to MA in terms of CO<sub>2</sub> adsorption capacity throughout the pressure range investigated. Meanwhile, zeolite 13X adsorbs more CO<sub>2</sub> up to ca. 10 bar, beyond which the CO<sub>2</sub> adsorption capacity of MA exceeds that of zeolite 13X. As pressure increases, physical properties of adsorbent such as surface area and pore volume become increasingly important for CO<sub>2</sub> capture, since high surface area means more adsorption sites available and large pore volume means more space for the storage of CO<sub>2</sub>. The advantage of larger pore volume in MA becomes more evident as pressure increases, leading to a higher CO<sub>2</sub> capture capacity of MA than that of zeolite 13X at high pressure condition (>10 bar).

In a post-combustion CO<sub>2</sub> capture system, the flue gas contains a high concentration of N<sub>2</sub> (ca. 70%), and CO<sub>2</sub> separation from the CO<sub>2</sub>/N<sub>2</sub> mixture should be considered. In order to evaluate the CO<sub>2</sub> separation efficiency of MA against N<sub>2</sub>, we carried out experiments in both static and flow adsorption systems. As shown in Fig. 3(e), the N<sub>2</sub> adsorption capacity at 298 K for MA is only about 1 mg/g<sub>adsorbent</sub>, which reflects a very high adsorption selectivity of CO<sub>2</sub>/N<sub>2</sub> (52 to 1 based on the amount of each gas adsorbed at  $P/P_0 = 1.0$ ) for MA. In a practical situation, the flue gas contains ca. 15% CO<sub>2</sub>. Therefore, we conducted a breakthrough experiment using a gas mixture mimicking the flue gas (15% CO<sub>2</sub>, N<sub>2</sub> as balance). As shown in Fig. 5, whereas N<sub>2</sub> appeared in the column downstream almost immediately after the process started due to a negligible adsorption capacity for N<sub>2</sub>, no CO<sub>2</sub> was detected downstream of the column until ca. 160 s.

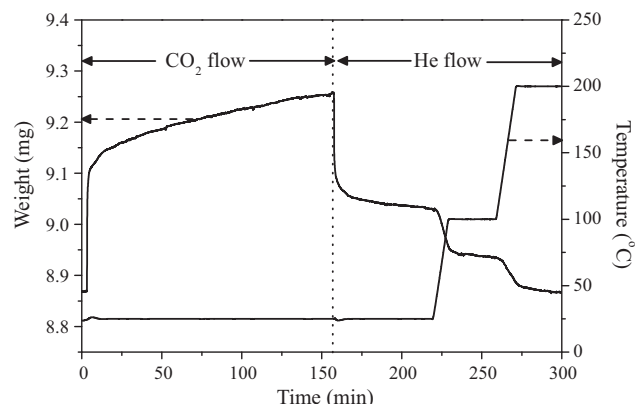


**Fig. 4.** High pressure CO<sub>2</sub> adsorption isotherms of (a) MA, (b) Zeolite 13X, (c) commercial  $\gamma$ -alumina, and (d) SBA-15 at 298 K.

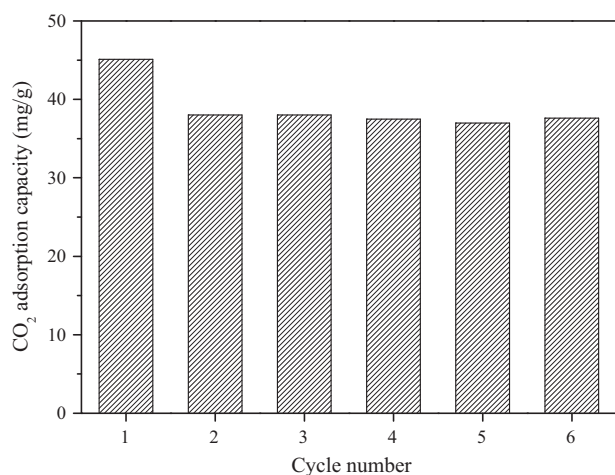


**Fig. 5.** Breakthrough curve of CO<sub>2</sub> (15% CO<sub>2</sub>, 85% balance N<sub>2</sub>) on MA.

In order to save energy in the system operation, the adsorbed CO<sub>2</sub> should be easily desorbed in an adsorbent during use of a multi-cycle adsorbent. Desorption performance of MA under a temperature swing was thus examined using a TGA unit. As shown in Fig. 6, about 60% of CO<sub>2</sub> can be easily desorbed at 25 °C by only a He gas purge. More than 80% CO<sub>2</sub> was desorbed at 100 °C and the remaining CO<sub>2</sub> was almost completely desorbed at 200 °C. This is consistent with the heat of adsorption values obtained above (insert in Fig. 3). CO<sub>2</sub> desorbed at high temperature corresponds to



**Fig. 6.** CO<sub>2</sub> desorption behavior of MA.



**Fig. 7.** Recycle runs of CO<sub>2</sub> by MA (adsorption at 25 °C for 150 min and desorption at 100 °C for 30 min).

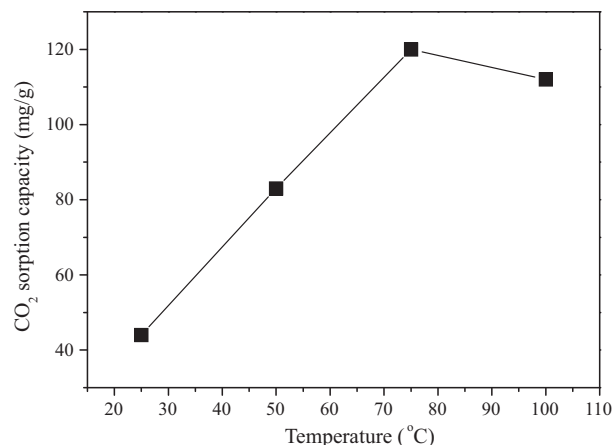
the strongly adsorbed CO<sub>2</sub> by the small number of strong chemical adsorption sites on the MA surface, where high heat of adsorption values were obtained, while the CO<sub>2</sub> desorbed at 25 °C by He gas purge indicates that most of the adsorption sites on the MA surface are weakly bound physical adsorption sites for CO<sub>2</sub>, which corresponds to the low heat of adsorption.

Finally, the stability of MA as a CO<sub>2</sub> adsorbent was investigated by multiple CO<sub>2</sub> adsorption–desorption runs using the same TGA unit, and the results are shown in Fig. 7. We adopted 100 °C as the desorption temperature considering the marginal increase of CO<sub>2</sub> recovery and the high energy cost demanded at 200 °C. Full CO<sub>2</sub> adsorption capacity was achieved in the first cycle by the fresh MA sample. As expected, the adsorption capacity of the second adsorption step decreased compared to the initial adsorption capacity, as only ca. 80% of the captured CO<sub>2</sub> could be desorbed at the desorption temperature tested. Starting from the second cycle, however, MA showed virtually stable adsorption–desorption performance during 5 consecutive runs.

### 3.3. CO<sub>2</sub> sorption by PEI-impregnated MA

CO<sub>2</sub> capturing agent PEI was then additionally introduced to MA by an impregnation method. As reported earlier [17,19–21], the loading amount of PEI on a porous support has an important effect on the CO<sub>2</sub> sorption performance. In general, high loading of PEI is desirable to achieve high CO<sub>2</sub> sorption capacity; however, too much PEI would decrease the efficiency of the sorbent, since some PEI will be coated on the outer surface of the support and behave like a bulk phase material. Thus, the maximum allowable amount of PEI (ca. 46.5 wt%) was introduced to the pores of MA based on the pore volume of MA and the density of PEI. The resultant hybrid material was characterized by XRD (Fig. 1b) and N<sub>2</sub> adsorption–desorption isotherms (Fig. 2c), which confirmed the successful preparation of PEI-impregnated MA.

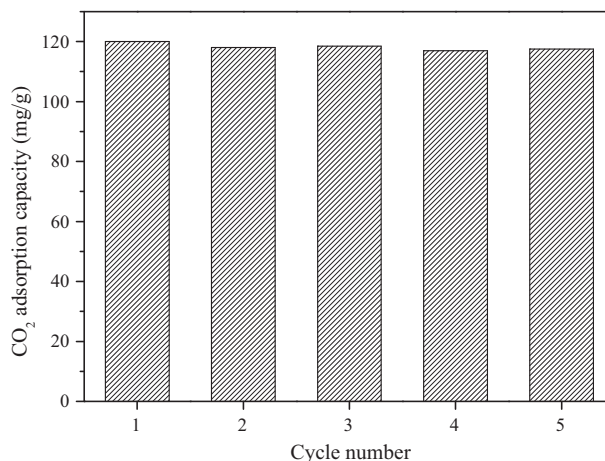
For this PEI-impregnated system, comparatively high temperature was needed for efficient carbon dioxide sorption. As the temperature increases, the amine groups in PEI become flexible and more CO<sub>2</sub>-affinity sites are exposed to CO<sub>2</sub>; the available pore space for CO<sub>2</sub> would also increase to some extent, leading to faster diffusion of CO<sub>2</sub> in the pore channels [17]. However, since the sorption process is exothermic, higher than optimal temperature favors the desorption process. Furthermore, since amine is introduced to the support by the impregnation method, the risk of amine evaporation from the support increases as the temperature is increased excessively. Therefore, initially, we investigated the effect of temperature



**Fig. 8.** CO<sub>2</sub> sorption performance of PEI/MA at different temperatures.

on the CO<sub>2</sub> capturing capacity to determine the optimum temperature for this system. As shown in Fig. 8, CO<sub>2</sub> capturing capacity increased with temperature and the highest CO<sub>2</sub> sorption capacity (120 mg/g<sub>sorbent</sub>) was established at 75 °C, which coincides with the optimum temperature reported by several researchers using PEI-impregnated mesoporous silica [17,19,21]. This CO<sub>2</sub> sorption capacity (120 mg/g<sub>sorbent</sub>) measured is comparable to that of the PEI-impregnated mesoporous silica previously reported [17]. The N amount in the PEI-impregnated MA sample was measured to be 157 mg/g<sub>sorbent</sub> by an EA, and the CO<sub>2</sub>/N ratio achieved was calculated to be 0.24. Compared to the stoichiometric CO<sub>2</sub>/N value of 0.5 in carbamate complex formation and the average value of CO<sub>2</sub>/N reported in an amine-grafted system on mesoporous silica [22], the CO<sub>2</sub>/N in PEI/MA appears to be lower. However, since the total amount of amine introduced by the PEI-impregnation method is far greater than that of an amine-grafted system, higher overall CO<sub>2</sub> capture capacity than that of an amine-grafted system can be produced.

The cyclic performance of PEI/MA is the most important criterion to determine whether MA can be a suitable support material for PEI. Thus, the performance of the PEI/MA in 5 consecutive CO<sub>2</sub> sorption-desorption runs was tested in terms of its stability. Both sorption and desorption runs were carried out at 75 °C [19–21]. As shown in Fig. 9, the PEI/MA demonstrated reversible and stable CO<sub>2</sub> sorption–desorption performance during 5 repeated runs without deterioration of the CO<sub>2</sub> capturing performance.



**Fig. 9.** Recycle runs of CO<sub>2</sub> by PEI/MA (adsorption at 75 °C for 150 min and desorption at 75 °C for 150 min).

The cyclic performance data of the PEI/MA indicate that MA here functions solely as a support material. After impregnating PEI into the MA, the mesopore channels are virtually filled with PEI, which was confirmed by the surface area (only 2 m<sup>2</sup>/g) and the residual pore volume (only 0.03 cm<sup>3</sup>/g) for the resultant hybrid material, as shown in Table 1. Thus, the CO<sub>2</sub> sorption process would be governed by the reaction of amine species with CO<sub>2</sub>. The contribution of adsorption sites in MA for CO<sub>2</sub> capture can be neglected in PEI/MA. Otherwise, the CO<sub>2</sub> would not be desorbed successfully at 75 °C (see Fig. 6).

#### 4. Conclusions

In summary, mesoporous alumina (MA) having high surface area and large pore volume was successfully synthesized by a simple sol–gel process. As-prepared MA alone showed a significant CO<sub>2</sub> adsorption capacity, and high adsorption selectivity of CO<sub>2</sub>/N<sub>2</sub>. MA maintained good stability in 5 adsorption–desorption runs. PEI-impregnated MA achieved high CO<sub>2</sub> sorption capacity and again performed satisfactorily during 5 consecutive adsorption–desorption test cycles, showing no deterioration. These results demonstrate that MA can be either directly used as a CO<sub>2</sub> adsorbent or as a support material for CO<sub>2</sub> sorption agents for the removal and recovery of CO<sub>2</sub> from power station flue gas.

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